# Coupled systems as quantum thermodynamic machines

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- Introduction
- Simple models of quantum heat engine
- Coupled systems as heat engines
- Refrigerator model
- Comparison of performances

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#### Quantum thermodynamics

To extend thermodynamics in quantum domain.

- Superposition and entanglement
- Quantum processes such as quantum adiabatic process
- A few particle system in a thermal environment

#### Quantum thermodynamics

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#### Models

Quantum thermodynamic machines

- Nikolaus Otto was the first person to build a working model of four-stroke engine in 1861.
- Four-stroke gasoline engines used nowadays are generally called Otto engines.

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# Classical Otto cycle



#### Work and Efficiency

$$egin{aligned} Q_1 &= C_{v}(T_1 - T_2'), & Q_2 &= C_{v}(T_2 - T_1') \ W &= Q_1 + Q2 \ \eta &= rac{W}{Q_1} &= 1 - rac{T_1'}{T_1} &= 1 - \left(rac{V_1}{V_2}
ight)^{(\gamma-1)}. \end{aligned}$$

# MASER as a heat engine



Figure : Three level MASER as a heat engine <sup>1</sup>

$$\eta_M = 1 - \frac{\nu_2}{\nu_1} \le 1 - \frac{T_2}{T_1}$$

 $<sup>^1</sup>$  H. E. D. Scovil and E. O. Schulz-DuBois, Phys. Rev. Lett. 2, 262 (1959).

#### Mean energy

$$U = \operatorname{Tr}(H\rho),$$

where H is the Hamiltonian and  $\rho$  is the density matrix.

#### First law of thermodynamics

$$dU = \operatorname{Tr}(H d\rho) + \operatorname{Tr}(\rho dH)$$
  
$$dQ = \operatorname{Tr}(H d\rho)$$
  
$$dW = \operatorname{Tr}(\rho dH)$$

= 990

#### Adiabatic process in thermodynamics

No heat is exchanged between the system and its surroundings, dQ = 0.

#### Quantum adiabatic process

Suppose the system is initially in the *n*th eigenstate of the initial Hamiltonian ( $H_{ini}$ ), then the Hamiltonian is changed gradually from  $H_{ini}$  to  $H_{fin}$ . According to Quantum adiabatic theorem, the system will remain in the *n*th eigenstate of the instantaneous Hamiltonian.

# A model of quantum heat engine



# Figure : Two level system as heat engine.

T. D. Kieu, Phys. Rev. Lett. 93, 140403 (2004).

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# Model of quantum heat engine



Figure : Harmonic oscillator as a model of heat engine.

#### Work and efficiency

$$egin{aligned} Q_h &= rac{\omega}{2} \left( ext{coth} \left[ rac{eta_{h\omega}}{2} 
ight] - ext{coth} \left[ rac{eta_{c}\omega'}{2} 
ight] 
ight) > 0 \ Q_c &= rac{\omega'}{2} \left( ext{coth} \left[ rac{eta_{c}\omega'}{2} 
ight] - ext{coth} \left[ rac{eta_{h\omega}}{2} 
ight] 
ight) < 0 \ W &= Q_1 + Q_2 > 0 \end{aligned}$$

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#### Condition for engine

$$egin{aligned} η_c \omega' \geq eta_h \omega \quad ext{and} \quad \omega > \omega' \ &\eta = 1 - rac{\omega'}{\omega} \leq 1 - rac{T_c}{T_h} \end{aligned}$$

# Comparison

#### Oscillator model

$$W^{
m os} = rac{(\omega - \omega')}{2} \left( \coth\left[rac{eta_h \omega}{2}
ight] - \coth\left[rac{eta_c \omega'}{2}
ight] 
ight)$$
  
 $\eta^{
m os} = rac{W^{
m os}}{Q_h^{
m os}} = 1 - rac{\omega'}{\omega}$ 

#### Spin model

$$W^{
m sp} = rac{(\omega - \omega')}{2} \left( \tanh\left[rac{eta_c \omega'}{2}
ight] - \tanh\left[rac{eta_h \omega}{2}
ight] 
ight)$$
 $\eta^{
m sp} = rac{W^{
m sp}}{Q_h^{
m sp}} = 1 - rac{\omega'}{\omega}$ 

$$\eta^{\mathrm{os}} = \eta^{\mathrm{sp}} \qquad W^{\mathrm{os}} > W^{\mathrm{sp}}$$

# Coupled systems as thermodynamic machines<sup>2</sup>

 $<sup>^2\</sup>text{G}.$  Thomas, M. Banik, and S. Ghosh, arXiv:1607.00994 [quant-ph] (2016).

# Coupled systems

$$\begin{aligned} H^{\rm os} &= \frac{p_1^2}{2m} + \frac{p_2^2}{2m} + \frac{m\Omega^2}{2}x_1^2 + \frac{m\Omega^2}{2}x_2^2 + 2\left(\frac{m\Omega}{2}\lambda_x x_1 x_2 + \frac{1}{2m\Omega}\lambda_p p_1 p_2\right) \\ H^{\rm os} &= \left(c_1^{\dagger}c_1 + c_2^{\dagger}c_2 + 1\right)\Omega + \frac{(\lambda_x + \lambda_p)}{2}(c_1^{\dagger}c_2 + c_1c_2^{\dagger}) \\ &+ \frac{(\lambda_x - \lambda_p)}{2}(c_1c_2 + c_1^{\dagger}c_2^{\dagger}) \end{aligned}$$

Heisenberg XY model

$$H^{\rm sp} = (S_1^+ S_1^- + S_2^+ S_2^- + 1)\Omega + \frac{(J_x + J_y)}{2}(S_1^+ S_2^- + S_1^- S_2^+) \\ + \frac{(J_x - J_y)}{2}(S_1^+ S_2^+ + S_1^- S_2^-)$$

# Co-ordinate Transformation

$$x_A = rac{x_1 + x_2}{\sqrt{2}}, \qquad x_B = rac{x_1 - x_2}{\sqrt{2}}; \ p_A = rac{p_1 + p_2}{\sqrt{2}}, \qquad p_B = rac{p_1 - p_2}{\sqrt{2}}.$$

$$H^{\rm os} = \frac{p_A^2}{2M_A} + \frac{M_A \Omega_A^2}{2} x_A^2 + \frac{p_B^2}{2M_B} + \frac{M_B \Omega_B^2}{2} x_B^2$$

$$\mathcal{H}^{\mathrm{os}} = \left(c_{\mathcal{A}}^{\dagger}c_{\mathcal{A}} + rac{1}{2}
ight)\Omega_{\mathcal{A}} + \left(c_{\mathcal{B}}^{\dagger}c_{\mathcal{B}} + rac{1}{2}
ight)\Omega_{\mathcal{B}}$$

$$\Omega_{A/B} = \sqrt{(\Omega \pm \lambda_p)(\Omega \pm \lambda_x)}.$$

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# Heat, work and efficiency

$$Q = \frac{\omega_A}{2} \left( \coth\left[\frac{\beta_h \omega_A}{2}\right] - \coth\left[\frac{\beta_c \omega'_A}{2}\right] \right) \\ + \frac{\omega_B}{2} \left( \coth\left[\frac{\beta_h \omega_B}{2}\right] - \coth\left[\frac{\beta_c \omega'_B}{2}\right] \right)$$

$$W = \frac{(\omega_A - \omega'_A)}{2} \left( \coth\left[\frac{\beta_h \omega_A}{2}\right] - \coth\left[\frac{\beta_c \omega'_A}{2}\right] \right) \\ + \frac{(\omega_B - \omega'_B)}{2} \left( \coth\left[\frac{\beta_h \omega_B}{2}\right] - \coth\left[\frac{\beta_c \omega'_B}{2}\right] \right) \\ W_A + W_B \qquad W_A \qquad W_B$$

$$\eta = \frac{\eta_A + \eta_B}{Q_A + Q_B}; \qquad \eta_A = \frac{\eta_A}{Q_A}; \qquad \eta_B = \frac{\eta_B}{Q_B}$$

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## Heat, work and efficiency

$$Q = \frac{\omega_A}{2} \left( \coth\left[\frac{\beta_h \omega_A}{2}\right] - \coth\left[\frac{\beta_c \omega'_A}{2}\right] \right) \\ + \frac{\omega_B}{2} \left( \coth\left[\frac{\beta_h \omega_B}{2}\right] - \coth\left[\frac{\beta_c \omega'_B}{2}\right] \right)$$

$$W = \frac{(\omega_A - \omega'_A)}{2} \left( \coth\left[\frac{\beta_h \omega_A}{2}\right] - \coth\left[\frac{\beta_c \omega'_A}{2}\right] \right) \\ + \frac{(\omega_B - \omega'_B)}{2} \left( \coth\left[\frac{\beta_h \omega_B}{2}\right] - \coth\left[\frac{\beta_c \omega'_B}{2}\right] \right) \\ \eta = \frac{W_A + W_B}{Q_A + Q_B}; \qquad \eta_A = \frac{W_A}{Q_A}; \qquad \eta_B = \frac{W_B}{Q_B}$$

 $\min\{\eta_A, \eta_B\} \le \eta \le \max\{\eta_A, \eta_B\}$ 

 $\min\{\eta_A, \eta_B\} \le \eta \le \max\{\eta_A, \eta_B\}$ 

When the Hamiltonian of the coupled system (at all stages of the cycle) can be decoupled (as two independent modes) in some suitably chosen co-ordinate system, then the efficiency of the coupled system is bounded (both from above and below) by the efficiencies of the independent modes, provided both the modes work as engines.

## XX-model

Now we consider the following case  $\lambda_x = \lambda_p = \lambda_J$  and  $J_x = J_y = \lambda_J$ .

$$H^{\rm os} = (\Omega + \lambda_J)(c_A^{\dagger}c_A + \frac{1}{2}) + (\Omega - \lambda_J)(c_B^{\dagger}c_B + \frac{1}{2})$$
$$H^{\rm sp} = (\Omega + \lambda_J)(S_A^{+}S_A^{-} + \frac{1}{2}) + (\Omega - \lambda_J)(S_B^{+}S_B^{-} + \frac{1}{2})$$

Consider the cycle  $\Omega:\omega\to\omega'\to\omega$ 

$$\eta_A = \frac{(\omega - \omega')}{(\omega + \lambda_J)}$$
 and  $\eta_B = \frac{(\omega - \omega')}{(\omega - \lambda_J)}$ 

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$$\begin{split} \eta^{\rm os} &= 1 - \frac{\omega'}{\omega} + \frac{\gamma \left( T_c {\rm csch}^2 \left[ \frac{\omega}{2T_h} \right] - T_h {\rm csch}^2 \left[ \frac{\omega'}{2T_c} \right] \right) \lambda_J^2}{2 \left( {\rm coth} \left[ \frac{\omega}{2T_h} \right] - {\rm coth} \left[ \frac{\omega'}{2T_c} \right] \right)} \\ &+ O[\lambda_J^4] \end{split}$$

$$\begin{split} \eta^{\rm sp} &= 1 - \frac{\omega'}{\omega} + \frac{\gamma \left( T_h {\rm sech}^2 \left[ \frac{\omega'}{2T_c} \right] - T_c {\rm sech}^2 \left[ \frac{\omega}{2T_h} \right] \right) \lambda_J^2}{2 \left( \tanh \left[ \frac{\omega}{2T_h} \right] - \tanh \left[ \frac{\omega'}{2T_c} \right] \right)} \\ &+ O[\lambda_J^4] \end{split}$$

$$\eta^{\rm os} - \eta^{\rm sp} = \gamma \left( T_c \operatorname{csch} \left[ \frac{\omega}{T_h} \right] + T_h \operatorname{csch} \left[ \frac{\omega'}{T_c} \right] \right) \lambda_J^2 > 0$$

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**Figure**: The two dotted curves show the upper bound  $(\eta_B)$  and lower bound  $(\eta_A)$ . The continuous curve represents the efficiency of the coupled oscillator. Efficiency of the coupled spin system is denoted by the dashed curve. When the upper bound reaches Carnot value,  $\eta_B = 1 - T_c / T_h$  for  $\lambda_J = \lambda_c$  (represented by vertical dashed-dotted line), then we get  $\eta^{OS} = \eta^{SP} = \eta_A$ . Here we take  $T_h = 2$ ,  $T_c = 1$ ,  $\omega = 4$  and  $\omega' = 3$ .

# Maximum work

$$W = W_{A} + W_{B} = \frac{(\omega_{A} - \omega'_{A})}{2} \left( \coth\left[\frac{\beta_{h}\omega_{A}}{2}\right] - \coth\left[\frac{\beta_{c}\omega'_{A}}{2}\right] \right) \\ + \frac{(\omega_{B} - \omega'_{B})}{2} \left( \coth\left[\frac{\beta_{h}\omega_{B}}{2}\right] - \coth\left[\frac{\beta_{c}\omega'_{B}}{2}\right] \right)$$
  
where  $\omega_{A} = \omega_{A}(\omega, \lambda_{x}, \lambda_{p}), \ \omega_{B} = \omega_{B}(\omega, \lambda_{x}, \lambda_{p}), \ \omega'_{A} = \omega'_{A}(\omega', \lambda_{x}, \lambda_{p}), \text{ and} \\ \omega'_{B} = \omega'_{B}(\omega', \lambda_{x}, \lambda_{p})$ 

Suppose  $W_A$  is maximum, when  $\omega_A = \omega_A *$  and  $\omega'_A = \omega'_A *$ . If the subsystem A provides subsystem work, then the work obtained from the subsystem B may not be optimal. Therefore we have

$$W_{\lambda \neq 0}^{\max} \leq W_{\lambda = 0}^{\max}$$

# Refrigerator model



Figure : Harmonic oscillator as a model of refrigerator.

#### Work and COP

$$Q_{h} = \frac{\omega}{2} \left( \operatorname{coth} \left[ \frac{\beta_{h}\omega}{2} \right] - \operatorname{coth} \left[ \frac{\beta_{c}\omega'}{2} \right] \right) < 0$$
$$Q_{c} = \frac{\omega'}{2} \left( \operatorname{coth} \left[ \frac{\beta_{c}\omega'}{2} \right] - \operatorname{coth} \left[ \frac{\beta_{h}\omega}{2} \right] \right) > 0$$
$$W = Q_{1} + Q_{2} < 0$$

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#### Condition for refrigerator

$$\beta_c \omega' \leq \beta_h \omega$$
 and  $\omega > \omega'$ 

$$\zeta = \frac{Q_c}{|W|} = \frac{\omega'}{\omega - \omega'} \le \frac{T_c}{T_h - T_c}$$

#### $\min\{\zeta_A,\zeta_B\} \le \zeta \le \max\{\zeta_A,\zeta_B\}$

The global coefficient of performance (COP) is bounded (both from above and below) by the COPs of the independent modes.

### Coupled system as refrigerator



**Figure**: The upper bound  $(\zeta_A)$  and the lower bound  $(\zeta_B)$  are shown with the dotted curves. The continuous curve represents the COP of the coupled oscillator and COP of the coupled spin system is denoted by the dashed curve. The horizontal line represents the CoP of the coupled spin system is denoted by the dashed curve. The horizontal line represents the sound by  $\zeta_A$  and  $\zeta_B$ . The plot also shows that the global COP of the coupled spin system is bounded by  $\zeta_A$  and  $\zeta_B$ . The plot also shows that the global COP of the coupled spins is higher than that of the coupled oscillators for small values of  $\lambda_J$ . When the upper bound achieves Carnot value,  $\zeta_A = T_c / (T_h - T_c)$  for  $\lambda_J = \lambda_c'$  (vertical dashed-dotted line), then we get  $\zeta^{OS} = \zeta^{OS} = \zeta_B$ . Inset shows the enlarged region near  $\lambda_J = \lambda_c'$ . Here we take  $T_h = 2$ ,  $T_c = 1$ ,  $\omega = 5$  and  $\omega' = 2$ .

# XY model

Now we consider the following case  $\lambda_x = -\lambda_p = \lambda_J$  and  $J_x = -J_y = \lambda_J$ .



**Figure**: (a) The continuous and the dashed curves represent the efficiencies of coupled oscillators and coupled spins respectively. The efficiency of the uncoupled oscillator (or spin) is shown by the horizontal dotted line. The parameter values are  $T_h = 2$ ,  $T_c = 1$ ,  $\omega = 4$  and  $\omega' = 3$ . (b) The COPs of coupled oscillators and spins are shown by continuous and dashed curves respectively. Horizontal dotted line represents COP of uncoupled oscillator (or spin). Here we used  $T_h = 2$ ,  $T_c = 1$ ,  $\omega = 5$  and  $\omega' = 2$ .

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# Thank you all !!

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